

## **Analytical Methods Update**

# Dave Heinrichs Lawrence Livermore National Laboratory



### **Outline**

- Analytic benchmarks
- Alpha particle transport
- Deuteron transport
- Advance (with BNL)
- SQA



COG11.1 will be provided to RSICC in advance of ICNC



## Analytic benchmarks completed in FY-2014

### Kobayahsi

### Cylinder



NUCLEAR SCIENCE COMMITTEE

### 3-D RADIATION TRANSPORT BENCHMARK PROBLEMS AND RESULTS FOR SIMPLE GEOMETRIES WITH VOID REGIONS

Keisuke Kobayash Naoki Sugimura Yasımobu Nagaya

November 2000

NUCLEAR ENERGY AGENCY ORGANISATION FOR ECONOMIC CO-OPERATION AND DEVELOPMENT

NUCLEAR SCIENCE AND ENGINEERING: 84, 79-82 (1983) The Critical Problem for an Infinite Cylinder J. R. Thomas, Jr. and J. D. Southers Virginia Polytechnic Institute and State University Nuclear Engineering Group, Blacksburg, Virginia 24061 C. E. Siewert North Carolina State University Raleigh, North Carolina 27650 Received November 18, 1982 Accepted January 1, 1983 The  $F_N$  method is used to compute the critical radius and the flux distribution for a bare cylinder of infinite length. With modest computational effort, the developed solution techniaue, though approximate, yields results accurate to at least six significant figures. I. INTRODUCTION isotropic. In this work we seek, for a given value of c > 1, the critical radius R and the resulting non-The integral equation for the neutron flux disnegative neutron flux  $\phi(r)$ ,  $r \in [0,R]$  that satisfies tribution  $\phi(r)$  in a bare homogeneous right circular cylinder of infinite length and radius R was written Following Mitsis,1 we let by Mitsis1 for the case of no inhomogeneous source  $\Phi(r,\mu) = c \left[ K_0(r/\mu) \int_{-\infty}^{\infty} t \phi(t) I_0(t/\mu) dt \right]$  $\phi(r) = c \int_0^1 \left[ K_0(r/\mu) \int_0^r t \phi(t) I_0(t/\mu) dt \right]$ +  $I_0(r/\mu)$   $\int_{-R}^{R} t\phi(t) K_0(t/\mu) dt$  $+I_0(r/\mu)\int_r^R t\phi(t)K_0(t/\mu)dt \left| \frac{d\mu}{\mu^2} \right|$  $\phi(r) = \int_{-1}^{1} \Phi(r, \mu) \frac{d\mu}{\mu^{2}}.$ where  $I_0(x)$  and  $K_0(x)$  denote modified Bessel functions<sup>2</sup> and c is the mean number of secondary Differentiating Eq. (2), we find that  $\Phi(r,\mu)$  for  $\mu \in [0,1]$  and  $r \in [0,R]$  satisfies neutrons per collision. Equation (1) is, of course, based on a one-speed model, and we have assumed that the redistribution of secondary neutrons is  $\left(\frac{\partial^2}{\partial r^2} + \frac{1}{r}\frac{\partial}{\partial r} - \frac{1}{u^2}\right)\Phi(r,\mu) = -c\int_{-r}^{1}\Phi(r,\mu')\frac{d\mu'}{u'^2}$  (4) <sup>1</sup>G. J. MITSIS, "Transport Solutions to the Mono-energetic Critical Problems," ANL-6787, Argonne National Laboratory (1963).
Mathematical Countries AMS 57, subject to the conditions that  $\Phi(0,\mu)$  is bounded and Handbook of Mathematical Functions, AMS-55, M.  $K_1(R/\mu)\Phi(R,\mu) + \mu K_0(R/\mu)\frac{\partial}{\partial r}\Phi(r,\mu)|_{r=R}=0$ , ABRAMOWITZ and I. A. STEGUN, Eds., U.S. National  $\mu \in [0.11]$  (5)

NSE 84 79-82 (1983)

J:\Back-and-forth approximation\Keff\_Alpha-2012-eng.doc Back-and-forth approximation,  $k_{eff}$  and  $\lambda$ V.M. Shmakov RUSSIAN FEDERAL NUCLEAR CENTER -Zababakhin All-Russia Research Institute of Applied Physics The back-and-forth approximation is a very simple neutron transport model that helps get a number of analytical solutions which qualitatively describe the actual characteristics of planar, cylindrical and spherical systems with fissile material. The model allows its absolutely accurate implementation in Monte Carlo codes and can be used to test the algorithms which do not treat geometry or interaction data. 1. Fundamental assumptions and definitions There are three fundamental assumptions in the back-and-forth approximation: (1) nuclear interaction with matter is treated in a one-group approximation; (2) neutrons are tracked in 1D geometry and (3) neutrons are allowed to move only in back and forth directions and this is exactly from what the approximation is named. In 1D geometries (plane, cylinder and sphere) neutrons are only allowed to move in two directions along straight lines, specifically normal's to the plane, the cylinder and the sphere. The same limitation on neutron directions applies to the neutron source and secondary neutrons from fission and scattering. Reference [1] describes the Schwarzschild approximation for photon transport. It is also referred to as back-and-forth. However, it differs from that one for neutrons because it assumes the isotropic scattering of photons in the forth and back hemispheres but with different weights. Reference [11] offers a two-flux approximation for descending and reflected flow of radiation in plane atmospheres. This method aims at getting simple analytical solutions for the fluxes. The scattering indicatrix is approximated by a sum of the delta-function and two terms of the Legendre polynomials. In the backand-forth approximation the scattering and fission indicatrix is approximated by a superposition of two In a one-group approximation the transport equation is written as [2,3]  $\frac{\partial N(x,\mu,t)}{\partial x} + \overrightarrow{\Omega} \cdot \overrightarrow{\nabla} \upsilon N(x,\mu,t) = -\rho \sigma_i \upsilon N(x,\mu,t) + \sum_{i=1}^{s-1} \rho \sigma_i (\mu' \to \mu) \cdot \nu_i \upsilon N(x,\mu',t) d\mu' + So \, (1.1)$ Here x denotes, in a unique manner, coordinates for all geometries, So is the source,  $\mu'$  and  $\mu$  are cosine angles between the neutron direction and the appropriate normal before and after collision, and i is reaction type (fission, absorption, scattering etc). In the back-and-forth model, the differential operator  $\vec{\Omega}\vec{\nabla}$  (divergent form) reads as [2, p. 46-48] for cylindrically symmetric geometry, and for spherically symmetric geometry Figures 1-3 show the angle between the direction of the scattered neutron and the normal in different geometries. In this model its cosine is only allowed to take two values:  $\mu = \pm 1$ . We will see later that this gives zero for the second operators with  $\frac{\partial}{\partial u}$  for cylindrically and spherically symmetric geometries, i.e., they can be omitted in the operator  $\vec{\Omega} \vec{\nabla}$ 

Unpublished manuscript (2012)

NSC-DOC2000-4 (2000)

COG results published by Ed Lent as LLNL-TR-648225, Three Analytic Benchmarks in COG, and presented at the NCSP TPR at LANL. COG results were generally excellent.



## Analytic benchmarks in progress

Data Bank

ISBN 978-92-64-99056-2 NEA/DB/DOC(2008)1

### Analytical Benchmarks for Nuclear Engineering Applications

Case Studies in Neutron Transport Theory

#### B.D. Ganapol

Department of Aerospace and Mechanical Engineering University of Arizona

with Forewords by

Paul F. Zweifel
Richard Sanchez and Norman J. McCormick

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NUCLEAR ENERGY AGENCY
ORGANISATION FOR ECONOMIC CO-OPERATION AND DEVELOPMENT

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## Infinite medium slowing down benchmarks

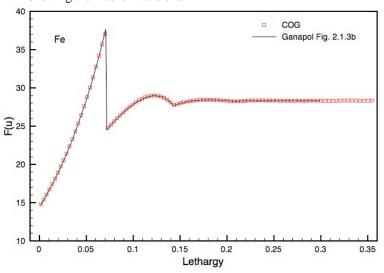
#### NEUTRON SLOWING DOWN AND THERMALIZATION

Benchmarks 2.1: Neutron slowing down in an infinite medium without spatial dependence and with constant cross sections.

Benchmark 2.1.2: Collision density vs. lethargy for neutrons slowing down in He.

| Lethargy | Ganapol<br>Table2.1.2 | COG     | sd(COG) | COG/<br>Ganapol | sd(COG)/<br>Ganapol |
|----------|-----------------------|---------|---------|-----------------|---------------------|
| 0.51083  | 2.08262               | 2.08290 | 0.00112 | 1.00013         | 0.00054             |
| 1.17057  | 2.26445               | 2.26580 | 0.00084 | 1.00060         | 0.00037             |
| 1.46840  | 2.34089               | 2.34070 | 0.00073 | 0.99992         | 0.00031             |
| 1.76624  | 2.36989               | 2.36990 | 0.00064 | 1.00000         | 0.00027             |
| 2.06407  | 2.33836               | 2.33810 | 0.00054 | 0.99989         | 0.00023             |
| 2.36191  | 2.35114               | 2.35130 | 0.00047 | 1.00007         | 0.00020             |
| 2.65974  | 2.35282               | 2.35300 | 0.00040 | 1.00008         | 0.00017             |
| 2.95758  | 2.35025               | 2.35040 | 0.00035 | 1.00006         | 0.00015             |
| 3.25541  | 2.35126               | 2.35150 | 0.00030 | 1.00010         | 0.00013             |
| 3.55325  | 2.35130               | 2.35240 | 0.00026 | 1.00047         | 0.00011             |
| 3.85108  | 2.35108               | 2.35270 | 0.00022 | 1.00069         | 0.00009             |

Benchmark 2.1.3b: The collision density vs. lethargy for Fe, showing the Placzek transient.



Slowing down benchmark results for 2.1.2, 2.1.3b, and 2.1.4 are excellent but .... minor <u>precision</u> issues at high lethargies.

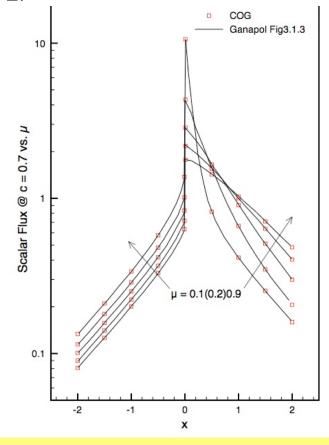


## 1-D transport benchmarks in planar geometry

Benchmarks 3.1: Neutron transport without energy loss in an isotropically scattering infinite medium including space dependence.

| ×     | Ganapol<br>Table 3.1.1 | COG<br>Scalar Flux | COG<br>sd(Scalar Flux) | COG/Ganapol<br>Scalar Flux | COG/Ganapol<br>sd(Scalar Flux) |
|-------|------------------------|--------------------|------------------------|----------------------------|--------------------------------|
| -5.00 | 1.02506E-01            | 1.0249E-01         | 3.2798E-05             | 0.99984                    | 0.00032                        |
| -4.00 | 1.73596E-01            | 1.7356E-01         | 4.2525E-05             | 0.99979                    | 0.00024                        |
| -3.00 | 2.94474E-01            | 2.9452E-01         | 5.5163E-05             | 1.00016                    | 0.00019                        |
| -2.00 | 5.01677E-01            | 5.0171E-01         | 7.1268E-05             | 1.00007                    | 0.00014                        |
| -1.00 | 8.66764E-01            | 8.6687E-01         | 9.2156E-05             | 1.00012                    | 0.00011                        |
| -0.01 | 1.66724E+00            | 1.6676E+00         | 1.2792E-04             | 1.00022                    | 0.00008                        |
| 0.01  | 2.71018E+00            | 2.7098E+00         | 1.3686E-04             | 0.99986                    | 0.00005                        |
| 1.00  | 2.17754E+00            | 2.1777E+00         | 1.3443E-04             | 1.00007                    | 0.00006                        |
| 2.00  | 1.42338E+00            | 1.4234E+00         | 1.1401E-04             | 1.00001                    | 0.00008                        |
| 3.00  | 8.83953E-01            | 8.8397E-01         | 9.2654E-05             | 1.00002                    | 0.00010                        |
| 4.00  | 5.36683E-01            | 5.3669E-01         | 7.3533E-05             | 1.00001                    | 0.00014                        |
| 5.00  | 3.22109E-01            | 3.2211E-01         | 5.7566E-05             | 1.00000                    | 0.00018                        |

Benchmark 3.1.3: Infinite 1-D planar medium, scattering is zero energy loss and isotropic in the LAB frame, point source of neutrons at x=0 beamed in the  $\mu$  direction. Determine scalar flux @ c=0.7 vs  $\mu$ .

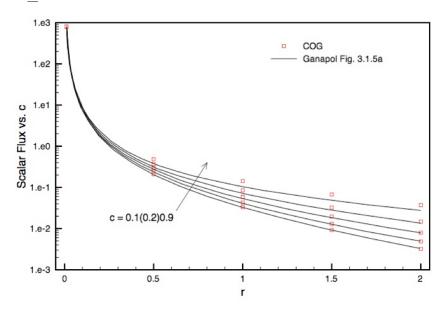


Infinite 1-D planar geometry transport benchmark results for 3.1, 3.1.2a, 3.1.2b, and 3.1.3 are <u>excellent</u> (as expected since 1-D cylindrical results reported in FY-2014 were also excellent).

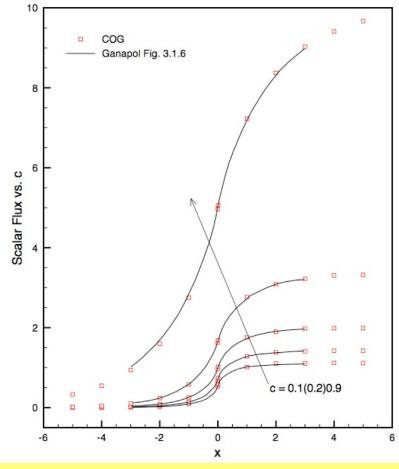


## 1-D transport benchmarks in spherical geometry

Benchmark 3.1.5a: Infinite 1-D spherical medium, scattering is zero energy loss and isotropic in the LAB frame, isotropic point source of neutrons at x = 0. Determine scalar flux vs c.



Benchmark 3.1.6: Infinite 1-D planar medium, scattering is zero energy loss and isotropic in the LAB frame, uniformly distributed source of neutrons in x > 0. Determine scalar flux vs c.

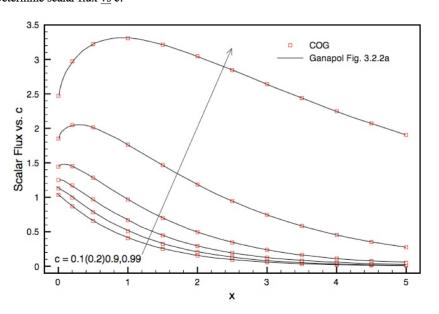


1-D spherical geometry transport benchmark results are either excellent (3.1.6) or have a possible issue with <u>precision</u> (3.1.5a, 3.1.5b).

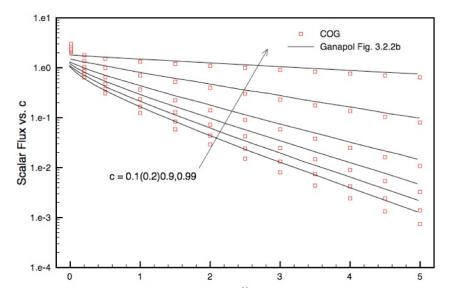


## Half-space "Milne" benchmarks

Benchmark 3.2.2a: Semi-infinite 1-D planar medium, scattering is zero energy loss and isotropic in the LAB frame, point source of neutrons at x = 0 beamed in x direction. Determine scalar flux vs c.



Benchmark 3.2.2b: Semi-infinite 1-D planar medium, scattering is zero energy loss and isotropic in the LAB frame, isotropic point source of neutrons at x = 0. Determine scalar flux vs c.

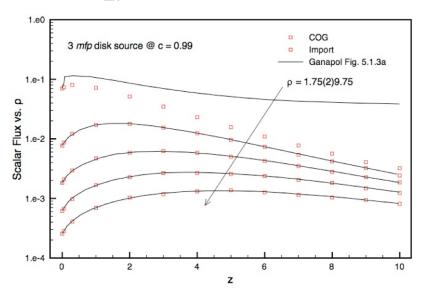


Semi-infinite transport benchmark results are either excellent (3.2.2a, 3.2.3, 3.3.1a, 3.3.1b, 3.3.2a, 3.3.2b) or in <u>error</u> (3.2.2b)

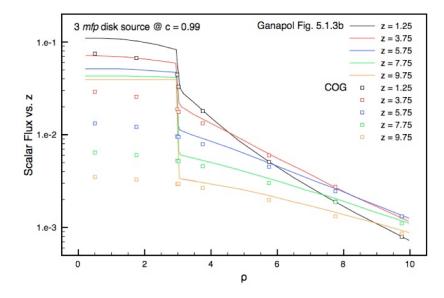


### Multidimensional benchmarks

Benchmark 5.1.3a: Semi-infinite 2-D medium, scattering is zero energy loss and isotropic in the LAB frame, disk source of radius 3 *mfp* at x = 0 beamed in x direction for c = 0.99. Determine scalar flux vs  $\rho$ .



Benchmark 5.1.3b: Semi-infinite 2-D medium, scattering is zero energy loss and isotropic in the LAB frame, disk source of radius 3 mfp at x = 0 beamed in x direction for c = 0.99. Determine scalar flux ys z.



Multidimensional benchmark results are either excellent (5.1, 5.1.2, 5.1.4a, 5.1.4b) or have serious <u>problems</u> (5.1.3a, 5.1.3b)



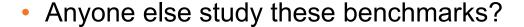
### Path forward

 Ed Lent is corresponding with the author to resolve noted discrepancies.



These benchmarks are actually code-to-code inter-comparisons.









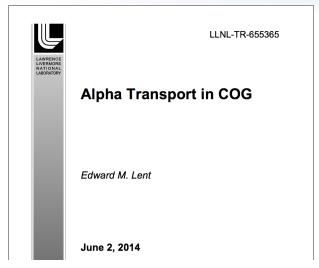


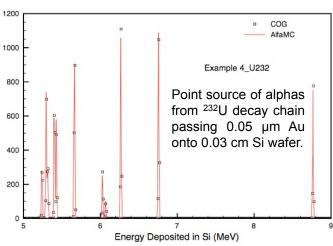






## Alpha particle transport in COG



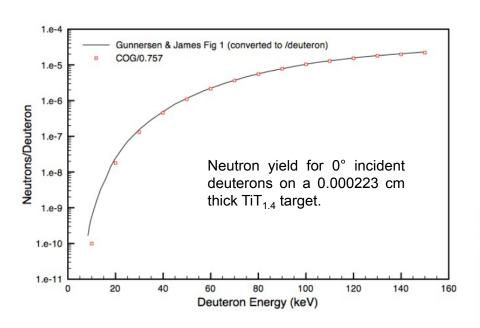


|        |         |           |             | rget (α,n) | Neutr | on Yie | lds, n | eutror |       |      |        |       |      |      |      |
|--------|---------|-----------|-------------|------------|-------|--------|--------|--------|-------|------|--------|-------|------|------|------|
|        |         |           | Calculation |            |       |        |        |        |       |      | Value: |       |      |      |      |
| Target | E (MeV) | COG-JENDL | COG-TENDL   |            | Ja83  | We82   | Ge80   | Sm80   | Ba79  | Bu79 | Ge75   | An71  | Go62 | Ru56 | Ro4  |
| Be     | 2.0     | 1.000     | 0.732       | 0.873      |       |        |        |        |       |      |        |       |      |      |      |
|        | 2.5     | 1.000     | 1.050       | 0.948      |       |        |        |        |       |      |        |       |      |      |      |
|        | 3.0     | 1.000     | 1.598       | 1.060      |       |        |        |        | 0.844 |      |        | 0.866 |      |      |      |
|        | 3.5     | 1.000     | 2.071       | 0.997      |       |        |        |        | 0.828 |      |        | 0.932 |      |      |      |
|        | 4.0     | 1.000     | 2.087       | 0.979      |       | 0.979  |        |        | 0.852 |      |        | 0.904 |      |      |      |
|        | 4.5     | 1.000     | 1.784       | 1.034      |       |        |        |        | 0.875 |      |        | 0.915 |      |      |      |
|        | 5.0     | 1.000     | 1.556       | 0.993      |       | 0.991  |        |        | 0.863 |      |        | 0.620 |      |      |      |
|        | 5.3     | 1.000     | 1.429       | 0.978      |       |        | 1.015  |        | 0.876 |      | 0.890  | 0.959 | 1.17 |      | 1.11 |
|        | 5.48    | 1.000     | 1.360       | 0.976      |       |        | 1.009  | 0.861  |       |      |        |       |      | 0.91 |      |
|        | 5.5     | 1.000     | 1.354       | 0.974      |       |        |        |        | 0.871 |      | 0.970  |       |      |      |      |
|        | 5.79    | 1.000     | 1.270       | 0.979      |       |        | 1.014  |        |       |      |        |       |      |      |      |
|        | 6.0     | 1.000     | 1.209       | 0.971      |       | 0.980  |        | 0.888  |       |      |        |       |      |      |      |
|        | 6.1     | 1.000     | 1.202       | 0.974      |       |        | 1.009  |        |       |      |        |       |      | 0.96 |      |
|        | 6.5     | 1.000     | 1.124       | 0.969      |       |        |        | 0.900  |       |      |        |       |      |      |      |
| С      | 3.0     | 1.000     | 1.400       | 1.450      |       |        |        |        | 1.200 |      |        |       |      |      |      |
|        | 3.5     | 1.000     | 1.472       | 1.417      |       |        |        |        | 1.111 |      |        |       |      |      |      |
|        | 4.0     | 1.000     | 2.289       | 1.500      | 1.026 | 1.132  |        |        | 1.105 |      |        |       |      |      |      |
|        | 4.5     | 1.000     | 2.864       | 1.477      | 1.045 |        |        |        | 1.068 |      |        |       |      |      |      |
|        | 5.0     | 1.000     | 2.867       | 1.350      | 1.017 | 1.083  |        |        | 1.050 |      |        |       |      |      |      |
|        | 5.3     | 1.000     | 2,356       | 1.310      |       |        |        |        |       |      |        |       | 1.3  |      | 1.03 |
|        | 5.5     | 1.000     | 2.168       | 1.327      | 0.944 |        |        |        | 1.028 |      |        |       |      |      |      |
|        | 6.0     | 1.000     | 1.710       | 1.204      |       | 0.925  |        |        | 0.914 |      |        |       |      |      |      |
|        | 6.5     | 1.000     | 1.646       | 1.250      |       |        |        |        | 0.969 |      |        |       |      |      |      |
| N      | 6.5     | 1.000     | 2.718       | 3.103      |       |        |        |        |       |      |        |       |      |      |      |
| Al     | 3.5     | 1.000     | 1.938       | 0.500      |       |        |        |        | 0.750 |      |        |       |      |      |      |
|        | 4.0     | 1.000     | 1.559       | 1.039      | 1.250 |        |        |        | 1.112 |      |        |       |      |      |      |
|        | 4.5     | 1.000     | 1.387       | 0.957      | 1.006 |        |        |        | 0.927 |      |        |       |      |      |      |
|        | 5.0     | 1.000     | 1.210       | 0.867      | 0.802 |        |        |        | 0.816 |      |        |       |      |      |      |
|        | 5.3     | 1.000     | 1.231       | 0.873      |       |        |        |        |       |      |        |       | 1.34 |      | 1.13 |
|        | 5.5     | 1.000     | 1.172       | 0.840      | 0.900 |        |        |        | 0.839 |      |        |       |      |      |      |
|        | 6.0     | 1.000     | 1.217       | 0.863      |       |        |        |        | 0.845 |      |        |       |      |      |      |
|        | 6.5     | 1.000     | 1.260       | 0.954      |       |        |        |        | 0.929 |      |        |       |      |      |      |
| Si     | 4.0     | 1.000     | 1.558       | 2.558      | 0.930 | 0.930  |        |        |       |      |        |       |      |      |      |
|        | 4.5     | 1.000     | 1.588       | 1.808      | 0.791 |        |        |        | 0.904 |      |        |       |      |      |      |
|        | 5.0     | 1.000     | 1.371       | 1.441      | 1.045 | 1.207  |        |        | 0.937 |      |        |       |      |      |      |
|        | 5.3     | 1.000     | 1.453       | 1.379      |       |        |        |        |       |      |        |       | 1.95 |      | 1.74 |
|        | 5.5     | 1.000     | 1.388       | 1.220      | 0.944 |        |        |        | 0.952 |      |        |       |      |      |      |
|        | 6.0     | 1.000     | 1.162       | 1.054      |       | 0.947  |        |        | 0.879 |      |        |       |      |      |      |
|        | 6.5     | 1.000     | 1.167       | 2.683      |       |        |        |        | 0.885 |      |        |       |      |      |      |

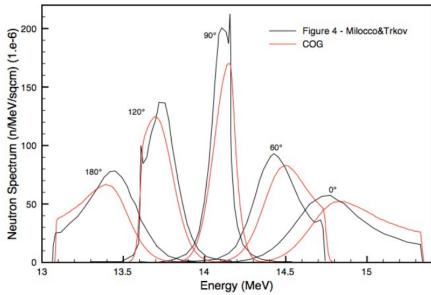
COG alpha transport is working well with the JENDL library which we have recommend for inclusion in ENDF/B. Need better experimental data and data for oxygen, fluorine, etc.



## Deuteron transport in COG



Comparison of calculated spectra from low voltage accelerated deuterons on titanium-tritium targets (see Hindawi, Publ. Corp., 2008, Article ID 340282, pp. 1-7).



Preliminary results look good. LLNL and Ohio integral pulsed sphere benchmarks are next.



### **ADVANCE**

- Automated Data Verification and Assurance for Nuclear Calculations Enhancement
- LLNL provided BNL with:
  - COG11.1 code
  - COG "Libmaker" files (also at RSICC)
  - 503 COG ICSBEP benchmarks
- BNL is now enabled to test changes to cross section evaluations by automatically building new COG libraries (in ACE or ENDF formats) and running the available benchmarks.
- LLNL will provide additional benchmarks





The goal: upon every commit to the ENDF subversion repository, run all available checks on the uploaded files, automatically.



### SQA

DOE G 414.1-4A DRAFT XX-XX-2015 B-3

Table B-1, Software Quality Assurance Work Activities and Corresponding Documentation for Demonstrating Compliance

|     | DOE O 414.1D SQA Work Activity  |   | SQA Documents  |
|-----|---|---|--|
| 1.  | Software Project Management and Quality<br>Planning   | - | Software Project Management Plan (SPMP) and/or Software Quality Assurance Plan (SQAP) Software Safety Plan   |
| 2.  | Software Risk Management  | - | Various document types can be used to cover risk management  |
| 3.  | Software Configuration Management   | - | Software Configuration Management Plan (SCMP) or related documents   |
| 4.  | Procurement and Supplier Management   | - | Contractual documents or other procurement and use agreement documentation   |
| 5.  | Software Requirements Identification and Management   | - | Software Requirements Specifications (SRS) or related document   |
| 6.  | Software Design and Implementation  | - | Software Design Description (SDD), Model Description, Programmer's Reference Manual, or other related documents  |
| 7.  | Software Safety   | - | SDD V Software Safety Analysis documentation V   |
| 8.  | Verification and Validation   | - | Verification and Validation Report  Test Case Description and Outcome Report; Other testing documents  |
| 9.  | Problem Reporting and Corrective Action   | - | Software Error Notification and Corrective Action Report   |
| 10. | Training of Personnel in the Design,<br>Development, Use and Evaluation of Safety<br>Software | - | User Instructions or User Manuals  Training Packages and User Qualification  |
| 11. | Model Validation and Evaluation   | - | Test results and evidence that code output was compared to experimental results or against equivalent output from an independent code and differences resolved |

New SQAP in development per ISQAP

New SCMP in development per ISQAP

Adding test cases with more detailed documentation.



### **Questions?**



#### COG11.1 - New Features, Data, V&V

Rich Buck, Dave Heinrichs, Chuck Lee, Ed Lent

Lawrence Livermore National Laboratory, 7000 East Avenue, L-198, Livermore, CA, 94550, USA work performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under Contract DE-ACS2-07NA2734-



#### **New Features**

CritDetVR – Enables hybrid criticality/shielding calculations for variance reduction of detector scores with no bias in the keff calculation.

**DFG** – Simulates delayed gamma emission from the fission product decay.

NRF – Simulates nuclear resonance fluorescence reactions for nuclear photon absorption and emission.

RadSrc – Automatic photon source calculation for gamma emission from  $\alpha$ -decay at a user-specified time (age).

**COGLEX** – Update includes dictionary entries for compounds with thermal scattering law.

#### **New Data Libraries**

NRF Library (Dr. Jim Hall, LLNL):

COGNRF

RadSrc Library (Dr. Ed Lent, LLNL):

**COGRS** 

DFG Libraries (Dr. Ed Lent, LLNL):

DFG.ENDFB7R1

DFG.JEFF3.1.1

**DFG.JENDL4** 

**Neutron Libraries:** 

ENDFB7R1, PT.ENDFB7R1, T.ENDFB7R1
JEFF3.1.2, PT.JEFF3.1.2, T.JEFF3.1.2

JENDL4

Dosimetry Library:

IRDFF1.02

Supported Library Formats:

ENDL ENDF ACE

GND (in progress)

Many, many older data libraries continue to be supported (e.g., JEF2.2, ENDF/B-V).

#### MC-to-S<sub>M</sub>

 $\mbox{\bf ARDRA}$  – COG geometry package is included in LLNL's modern massively parallel  $\mbox{\bf S}_{N}$  code with automatic meshing features.

#### V&V

**COG11BETA2** has been extensively tested using the following test suites:

Regression tests (11 cases)

ICSBEP criticality benchmarks (501 cases)

NRF tests (3 cases)

SINBAD shielding benchmarks (9 cases)

SILENE Activation benchmarks (11 cases)
PHOTONUCLEAR benchmarks (16)

KOBAYASHI exact solutions (in progress)

**CRITCYL** exact solutions (in progress)

#### Automation

LLNL is automating V&V code/data testing as described by M.-A. Descalle at ND2013. BNL is involved in a similar effort.

#### Website/Email

Please visit our website at <a href="http://cog.llnl.gov">http://cog.llnl.gov</a> and contact us at <a href="https://cog.llnl.gov">COG@llnl.gov</a>.





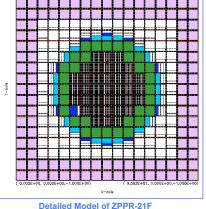
### **COG11.1 – Practical Applications**

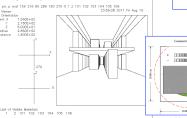
Rich Buck, Dave Heinrichs, Chuck Lee, Ed Lent

Lawrence Livermore National Laboratory, 7000 East Avenue, L-198, Livermore, CA, 94550, USA

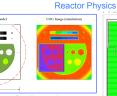








Storage Vault Model Shielding & Criticality Safety



Neutron Radiography

NURLEAR

TRANNO MODULE

CIGATIVATE

COS SOFTWARE

COS

Lawrence Livermore National Laboratory
Livermore, California

Practical User Training

Certificate of Completion

Your Name Here

Not successfully completed are introductory (CDL sure training current for ordinally suffer presentations) (CE-119-0416)

TOTAL TRAINING AND ADMINISTRATIONS (CE-119-0416)

Ministration Laboratory)

Fission Product Decay Gammas

Dose Assessment

LLNL-POST-644395

LLNL-POST-644394